

11-06-06

CofCA

G. Gregory Schivley schivley@hdp.com

November 3, 2006

Certificate

Director of the United States Patent and Trademark Office P.O. Box 1450 Alexandria, Virginia 22313-1450

Re:

Atty Docket No. 9319A-000222

U.S. Patent No. 6,979,374 / Issued: December 27, 2005

"MAGNETIC POWDER, MANUFACTURING METHOD OF MAGNETIC

POWDER AND BONDED MAGNETS"

Inventors: ARAI, et al.

Sir:

We have reviewed the above-indicated patent and have found several errors which appear to require a Certificate of Correction.

Enclosed herewith are an original and a copy of the Patent and Trademark Office Certificate of Correction form which we request be approved for the above-indicated patent.

Please charge \$100.00 to Epson R&D Deposit Account No. 50-3213 and any further fees which may be due. A duplicate copy of this sheet is enclosed.

Respectfully submitted,

EV 757 778 278 US

By:_

G. Gregory Sohivley

Reg. No. 27, 282

HARNESS, DICKEY & PIERCE, P.L.C. 🔻

Attorneys for Patentee

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CERTIFICATE OF MAILING

I hereby certify that this correspondence is being deposited with the United States Postal Service as express mail in an envelope addressed to: Director of the United States Patent Trademark Office, P.O. Box, 1450, Alexandria, Virginia 22213-1450 on

Harness, Dickey & Pierce, P.L.C. Autorneys and Counselors

tropolitan:

Detroit, MI

St. Louis, MO

Washington, DC

PATENT NO: 6,979,374

DATED: December 27, 2005

INVENTOR(S): Arai, et al.

It is certified that error appears in the above-identified patent and that said Letters Patent are hereby corrected as shown below:

Title Page, No. (56) References Cited

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Line 64, "(in" should be --in--.

Column 17

Line 29, "s" should be --a--.

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MAILING ADDRESS OF SENDER:

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PATENT NO. <u>6,979,374</u>

Page 1 of 6

PATENT NO: 6,979,374 DATED: December 27, 2005

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Column 17

Line 30, "reached" should be --reach--.

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Lines 63-64, "(BH)max" should be --(BH)max--.

Column 18 Line 38, "R_{CJ}" should be --H_{CJ}--.

Column 20

Line 8, "Wa₀₃" should be --W₀₃--.

Column 20

Table 2, Line 2, Col. 6, "(BH)_{max}/ ρ_2 " should be --(BH)_{max}/ ρ^2 --.

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PATENT NO. 6.979 374 1 3 2005

>Page 2 of 6

PATENT NO: 6,979,374

DATED: December 27, 2005

INVENTOR(S): Arai, et al.

It is certified that error appears in the above-identified patent and that said Letters Patent are hereby corrected as shown below:

Columns 20-22

Lines 44-34, Delete Claims 1-18 and insert:

-- 1. A magnetic powder comprising:

an alloy composition represented by $R_x(Fe_{1-a}Co_a)_{100-x-y-z}B_yM_z$ (where R is at least one rare-earth element selected from the group consisting of Nd and Pr, a ratio of Pr with respect to a total mass of R is in the range of 20-60%, M is at least one element selected from Ti, Cr, Nb, Mo, Hf, W, Mn, and Zr, x is 7.1 – 9.9 at%, y is 4.6-8.0 at%, z is 0.1-3.0 at %, and a is 0-0.30);

wherein the magnetic powder further comprises a composite structure having a soft magnetic phase and a hard magnetic phase;

an average particle size of the magnetic powder is 1-50 µm; and when the magnetic powder is mixed with a binding resin and then the mixture is subjected to compaction molding to form a bonded magnet having a density $\rho[Mg/m^3]$, a maximum magnetic energy product (BH)max[kJ/m³] of the bonded magnet at room temperature satisfies the relationship represented by the formula of (BH)max/ $\rho^2[x10^{-9}J\cdot m^3/g^2] \ge 2.40$, and the intrinsic coercive force H_{CJ} of the bonded magnet at room temperature is in the range of 430 – 750 kA/m.

2. The magnetic powder as claimed in claim 1, wherein the remanent magnetic flux density Br[T] of the bonded magnet at room temperature satisfies the relationship represented by the formula of Br/p[x10⁻⁶T·m³/g] \geq 0.125.

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Page 3 of 6 100 11 3 2006

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wherein the magnetic powder further comprises a composite structure having a soft magnetic phase and a hard magnetic phase;

an average particle size of the magnetic powder is 1-50 μ m; and when the magnetic powder is mixed with a binding resin and then the mixture is subjected to compaction molding to form a bonded magnet having a density p[Mg/m³], a remanent magnetic flux density Br[T] of the bonded magnet at a room temperature satisfies the relationship represented by the formula of Br/p [x10⁻⁶T·m³/g] \geq 0.125 and the intrinsic coercive force H_{CJ} of the bonded magnet at room temperature is in the range of 430 - 750 kA/m.

- 4. The magnetic powder as claimed in claim 1, wherein the magnetic powder has been obtained by milling a melt spun ribbon.
- 5. The magnetic powder as claimed in claim 4, wherein the thickness of the melt spun ribbon is 10 40µm.
- 6. The magnetic powder as claimed in claim 4, wherein the melt spun ribbon has been obtained by colliding a molten alloy of a magnetic material onto a circumferential surface of a cooling roll which is rotating to cool and then solidify the molten alloy.

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- 7. The magnetic powder as claimed in claim 6, wherein the cooling roll includes a roll base made of a metal or an alloy and an outer surface layer provided on an outer peripheral portion of the roll base to constitute the circumferential surface, in which the outer surface layer of the cooling roll has a heat conductivity lower than the heat conductivity of the roll base.
- 8. The magnetic powder as claimed in claim 7, wherein the outer surface layer of the cooling roll is formed of a ceramic.
- 9. The magnetic powder as claimed in claim 1, wherein the magnetic powder has been subjected to a heat treatment at least once during the manufacturing process or after the manufacture of the magnetic powder.
- 10. The magnetic powder as claimed in claim 1, wherein the mean crystal grain size of the magnetic powder is 5 50nm.
- 11. The magnetic powder as claimed in claim 3, wherein the magnetic powder has been obtained by milling a melt spun ribbon.
- 12. The magnetic powder as claimed in claim 3, wherein the thickness of the melt spun ribbon is 10 40µm.
- 13. The magnetic powder as claimed in claim 11, wherein the melt spun ribbon has been obtained by colliding a molten alloy of a magnetic material onto a circumferential surface of a cooling roll which is rotating to cool and then solidify the molten alloy.

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Page 5 of 6

NOV 11 3 2006

Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

(Also Form PTO-1050)

UNITED STATES PATENT AND TRADEMARK OFFICE CERTIFICATE OF CORRECTION

PATENT NO: 6,979,374

DATED: December 27, 2005

INVENTOR(S): Arai, et al.

It is certified that error appears in the above-identified patent and that said Letters Patent are hereby corrected as shown below:

- 14. The magnetic powder as claimed in claim 13, wherein the cooling roll includes a roll base made of a metal or alloy and an outer surface layer provided on an outer peripheral portion of the roll base to constitute the circumferential surface, in which the outer surface layer of the cooling roll has a heat conductivity lower than the heat conductivity of the roll base.
- 15. The magnetic powder as claimed in claim 14, wherein the outer surface layer of the cooling roll is formed of a ceramic.
- 16. The magnetic powder as claimed in claim 3, wherein the magnetic powder is constituted from a composite structure having a soft magnetic phase and a hard magnetic phase.
- 17. The magnetic powder as claimed in claim 3, wherein the magnetic powder has been subjected to a heat treatment at least once during the manufacturing process or after the manufacture of the magnetic powder.
- 18. The magnetic powder as claimed in claim 3, wherein the mean crystal grain size of the magnetic powder is 5 50nm.--

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Line 8, "Wao3" should be -- Wo3-.

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wherein the magnetic powder further comprises a composite structure having a soft magnetic phase and a hard magnetic phase;

an average particle size of the magnetic powder is 1-50 µm; and when the magnetic powder is mixed with a binding resin and then the mixture is subjected to compaction molding to form a bonded magnet having a density $\rho[Mg/m^3]$, a maximum magnetic energy product (BH)max[kJ/m³] of the bonded magnet at room temperature satisfies the relationship represented by the formula of (BH)max/ $\rho^2[x10^{-9}J \cdot m^3/g^2] \ge 2.40$, and the intrinsic coercive force H_{CJ} of the bonded magnet at room temperature is in the range of 430 – 750 kA/m.

2. The magnetic powder as claimed in claim 1, wherein the remanent magnetic flux density Br[T] of the bonded magnet at room temperature satisfies the relationship represented by the formula of Br/ ρ [x10-8T·m³/g] \geq 0.125.

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3. A magnetic powder comprising:

an alloy composition represented by $R_x(Fe_{1-a}Co_a)_{100-x-y-z}B_yM_z$ (where R is at least one rare-earth element selected from the group consisting of Nd and Pr, a ratio of Pr with respect to a total mass of R is in the range of 20-60%, M is at least one element selected from Ti, Cr, Nb, Mo, Hf, W, Mn, and Zr, x is 7.1 – 9.9 at%, y is 4.6 – 8.0 at%, z is 0.1 – 3.0 at%, and a is 0 – 0.30);

wherein the magnetic powder further comprises a composite structure having a soft magnetic phase and a hard magnetic phase;

an average particle size of the magnetic powder is 1-50 µm; and when the magnetic powder is mixed with a binding resin and then the mixture is subjected to compaction molding to form a bonded magnet having a density p[Mg/m³], a remanent magnetic flux density Br[T] of the bonded magnet at a room temperature satisfies the relationship represented by the formula of Br/p [x10-6T·m³/g] \geq 0.125 and the intrinsic coercive force H_{CJ} of the bonded magnet at room temperature is in the range of 430 - 750 kA/m.

- 4. The magnetic powder as claimed in claim 1, wherein the magnetic powder has been obtained by milling a melt spun ribbon.
- 5. The magnetic powder as claimed in claim 4, wherein the thickness of the melt spun ribbon is $10 40 \mu m$.
- 6. The magnetic powder as claimed in claim 4, wherein the melt spun ribbon has been obtained by colliding a molten alloy of a magnetic material onto a circumferential surface of a cooling roll which is rotating to cool and then solidify the molten alloy.

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- 8. The magnetic powder as claimed in claim 7, wherein the outer surface layer of the cooling roll is formed of a ceramic.
- 9. The magnetic powder as claimed in claim 1, wherein the magnetic powder has been subjected to a heat treatment at least once during the manufacturing process or after the manufacture of the magnetic powder.
- 10. The magnetic powder as claimed in claim 1, wherein the mean crystal grain size of the magnetic powder is 5-50nm.
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- 15. The magnetic powder as claimed in claim 14, wherein the outer surface layer of the cooling roll is formed of a ceramic.
- The magnetic powder as claimed in claim 3, wherein the magnetic powder is constituted from a composite structure having a soft magnetic phase and a hard magnetic phase.
- 17. The magnetic powder as claimed in claim 3, wherein the magnetic powder has been subjected to a heat treatment at least once during the manufacturing process or after the manufacture of the magnetic powder.
- The magnetic powder as claimed in claim 3, wherein the mean crystal grain size of the magnetic powder is 5 - 50nm.-

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